



Hussein Hanesch

PhD Thesis

**METHOD OF REDUCING HUB LOSSES OF PUSHER
AIR PROPELLERS WITH TANDEM BLADES OF
SMALL UAV**

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JUSTIFICATION RELEVANCE AND RESEARCH PROBLEMS

**FOR SMALL SIZE UAV
VERY IMPOTANT**



- Decreasing geometrical size of propeller (diameter)
- Increasing efficiency of propeller

**BENEFITS
OF TANDEM BLADE**

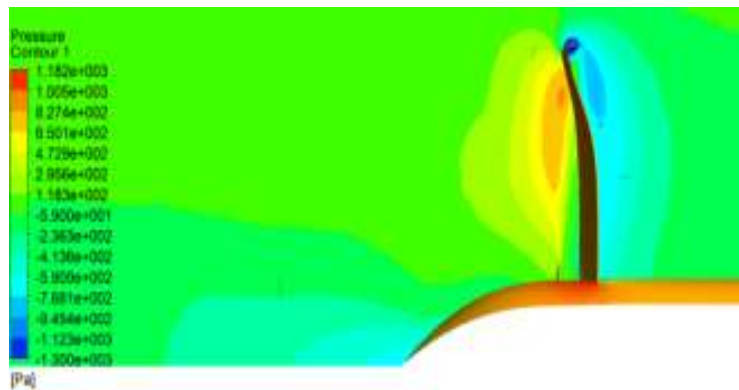


- Increasing aerodynamic loading of propeller blades
- Decreasing geometrical size of propeller (diameter)

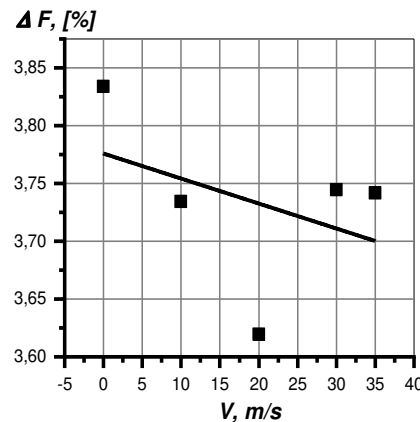
**DISADVANTAGES
OF TANDEM BLADE**



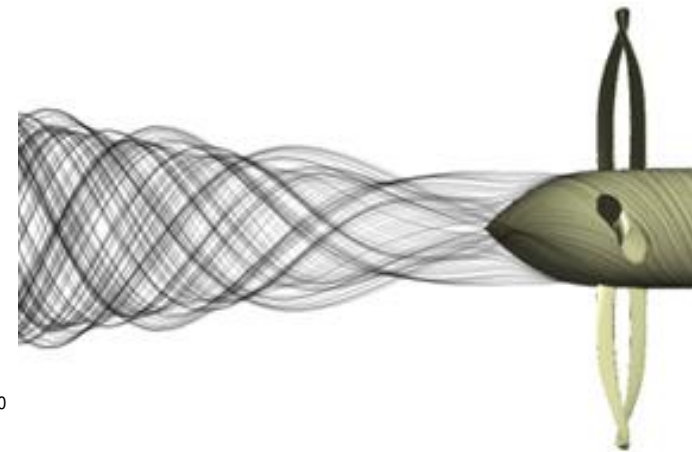
- Increasing level of tip and hub loses
- Increasing generating noise level (for unclosed blade)
- Difficult the blade pitch change mechanism



Contour of pressure distribution



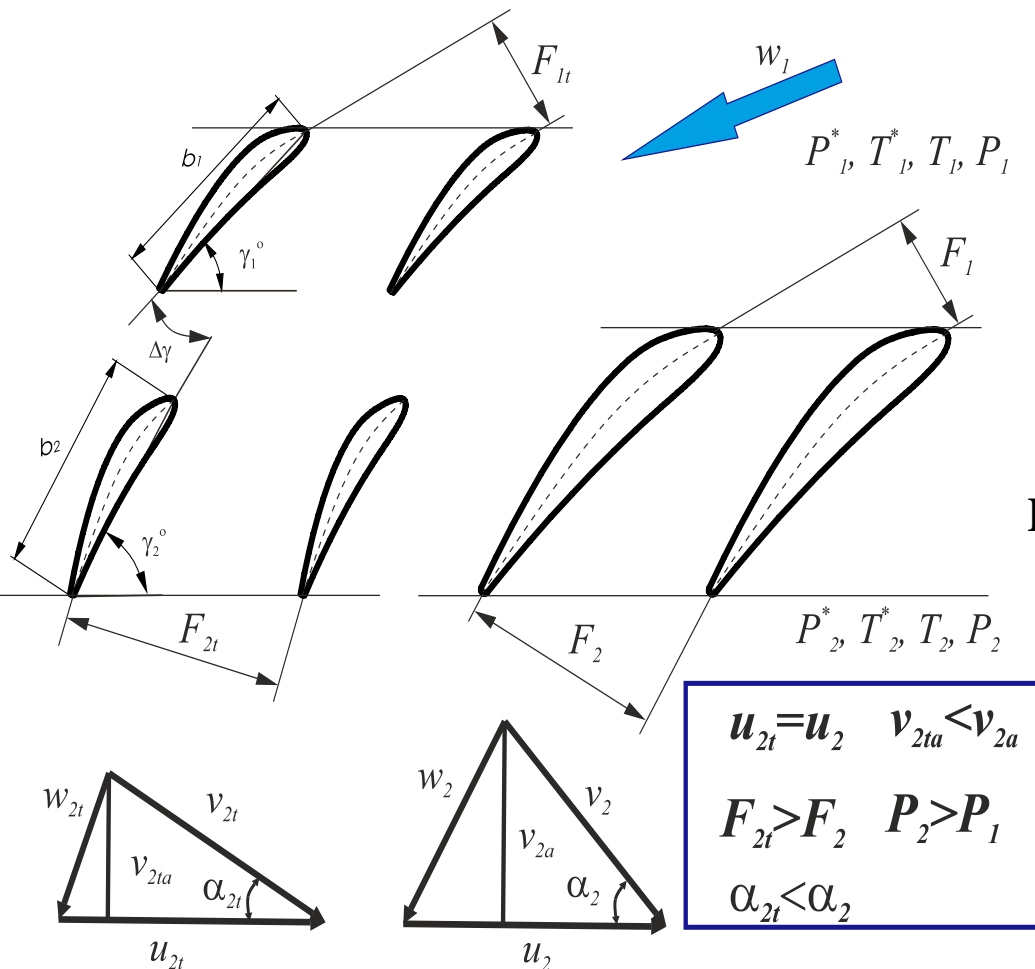
Axial force losses



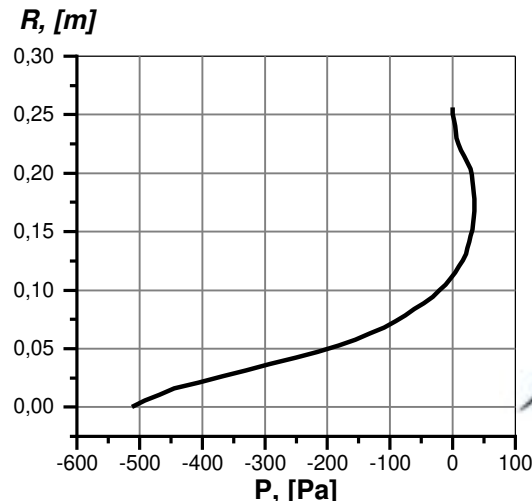
Structure of hub vortex



THE MAIN CAUSES OF THE HUB VORTEX INITIATION



Velocity triangle behind tandem and single blade rows propeller



Pressure distribution behind propeller hub

$$\frac{dp}{d\bar{r}} = \rho \frac{w_t^2}{\bar{r}}$$

pressure distribution
in the radial direction

$$p_0 = p_\infty - \rho \int_0^\infty \frac{w_t^2}{\bar{r}} d\bar{r}$$

pressure at the center
of vortex

$$p(r) = p_0 - \rho \int_0^r \frac{w_t^2}{\bar{r}} d\bar{r}$$

pressure in the
radial direction

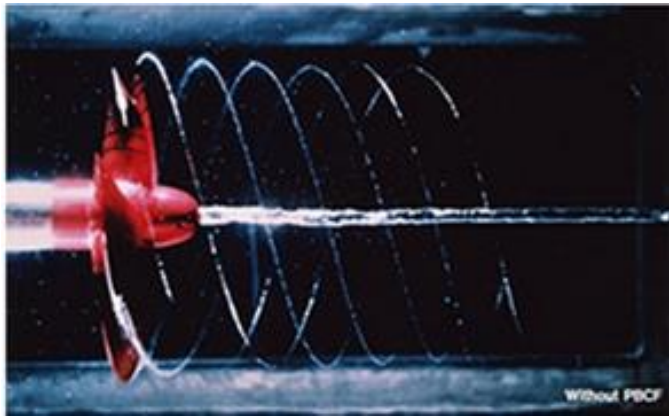
$$T_h = \frac{2\pi}{S_h} \int_0^{r_h} r p(r) dr$$

negative thrust of the
hub and spinner



THE MAIN WAYS TO REDUCE HUB VORTEX INTENSITY

Vortex flow behind the propeller



before installation of PBCF



after installation of PBCF



Propeller with
Boss Cap Fins

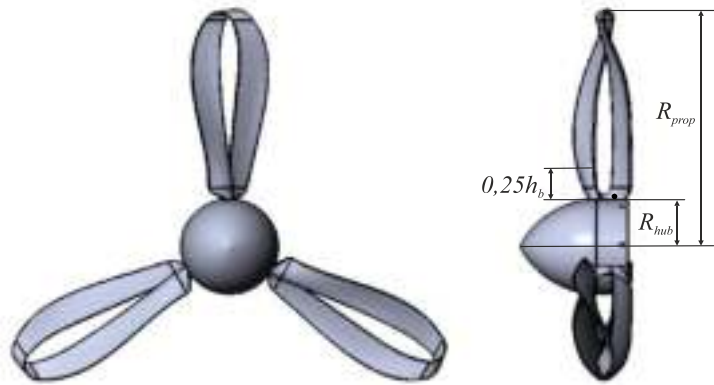


Rim driven fan

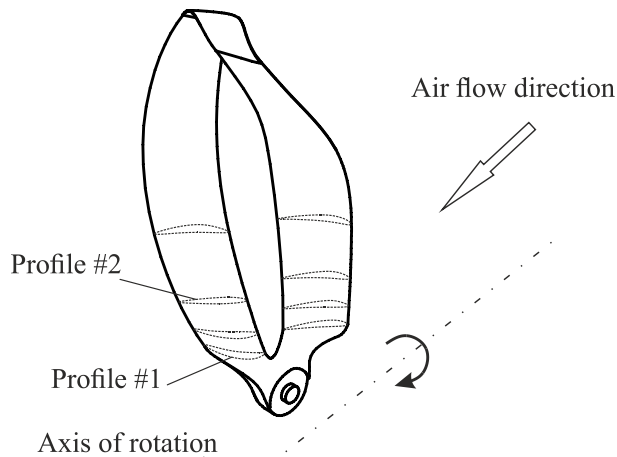




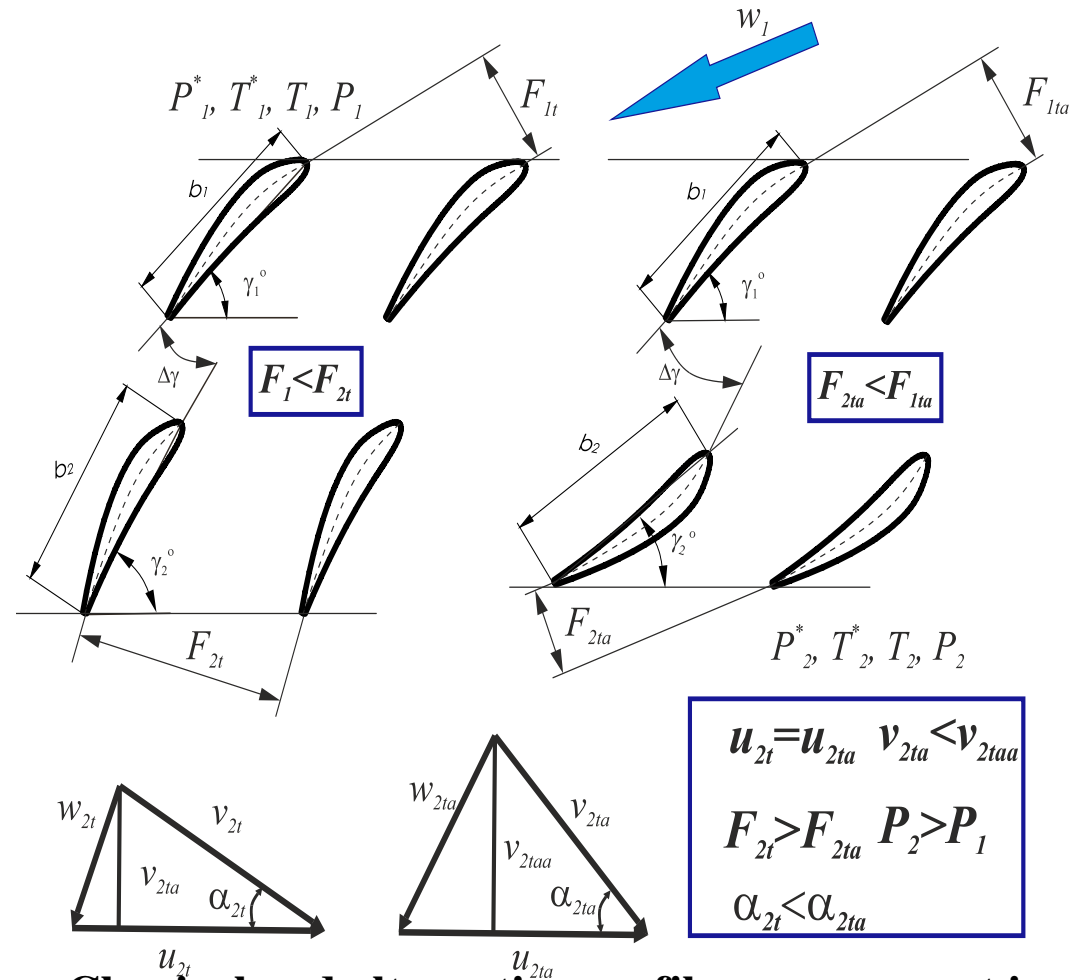
METHOD OF HUB VORTEX INTENSITY REDUCING



Object of investigation



The tandem propeller blade with alternative profiles arrangement



Classical and alternative profile arrangement in hub section of tandem propeller blade



METHODOLOGY OF TANDEM PROPELLER CHARACTERISTICS EXPERIMENTAL RESEARCH

Prop diameter - 406 mm

Hub diameter - 80 mm

RPM - 5000 rev/min

Blade number - 3

Advance ratio

$$J = \frac{V_{\infty}}{nD}$$

Trust coefficient

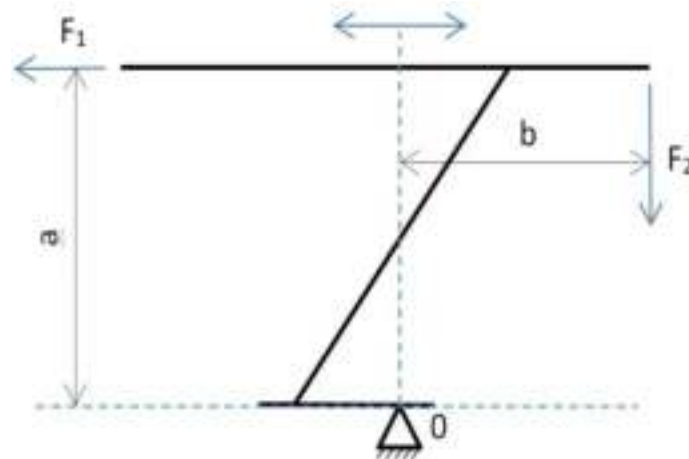
$$C_T = \frac{T_x}{\rho_{\infty} n^2 D^4}$$

Power coefficient

$$C_P = \frac{P_{shaft}}{\rho_{\infty} n^3 D^5}$$

Efficiency

$$\eta = \frac{T_x V_{\infty}}{P_{shaft}}$$



Chem of force balance

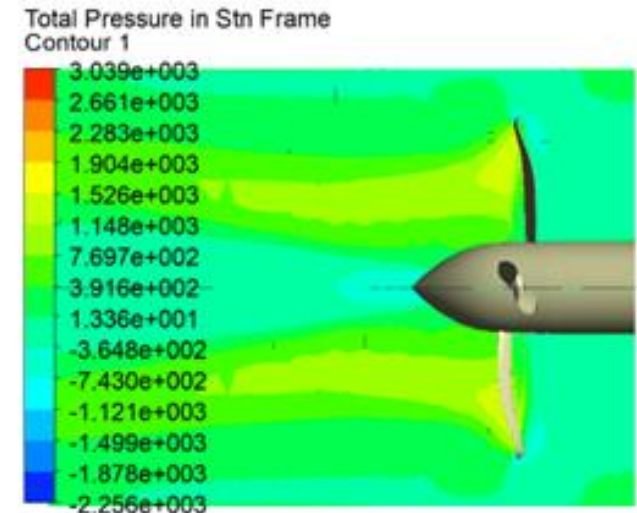
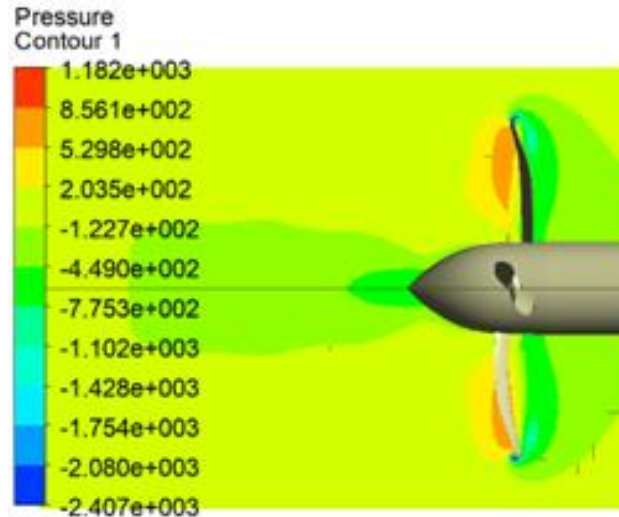




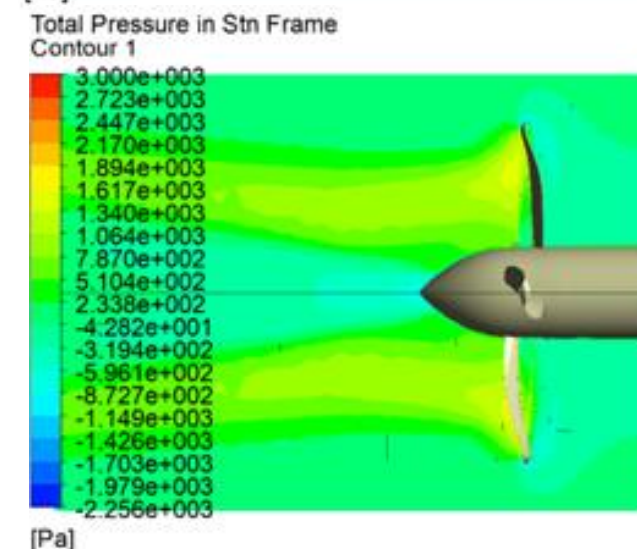
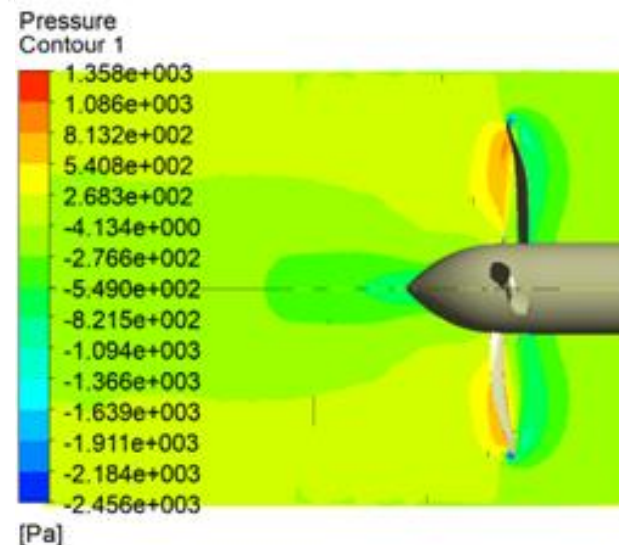
RESULTS OF TANDEM PROPELLER INVESTIGATIONS BEFOR MODIFICATION

Contour of
pressure and
total pressure
distribution
in the meridional
section of propeller

$$\Delta\gamma=0^\circ$$



$$\Delta\gamma=15^\circ$$

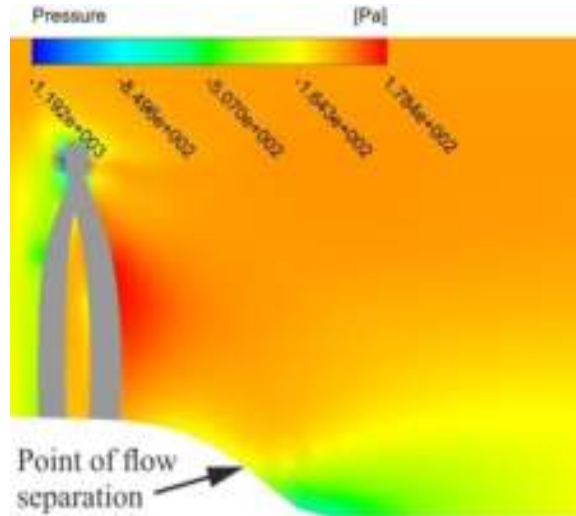




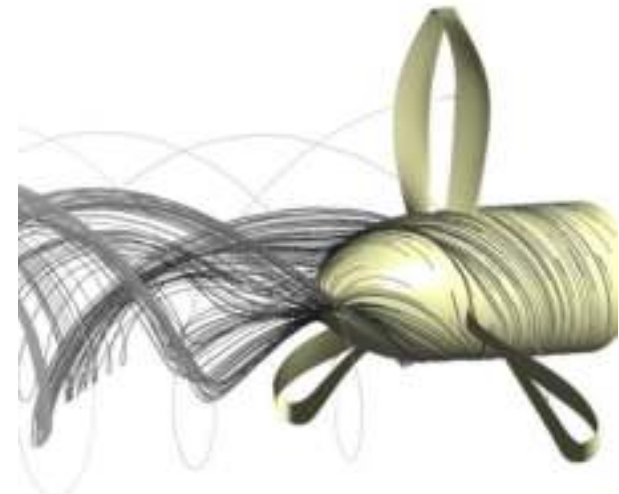
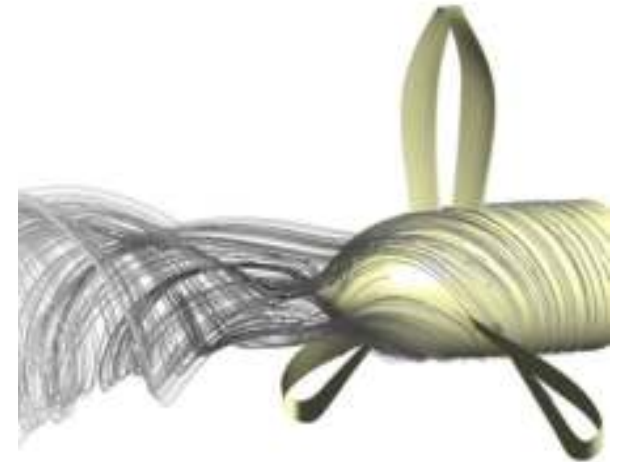
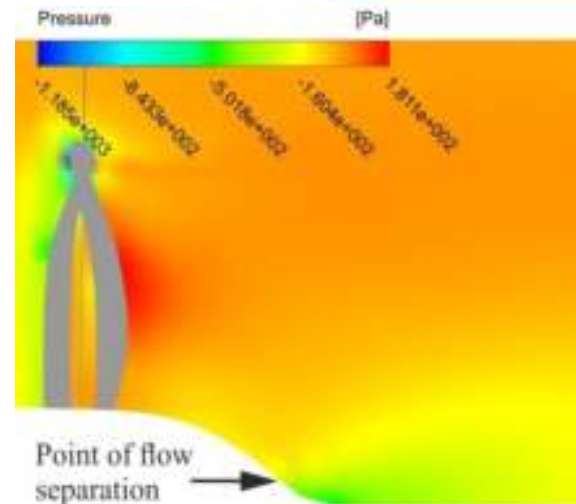
CHARACTERISTICS OF TANDEM PROPELLER AFTER MODIFICATION AND OPTIMIZATION PROFILE ARRANGEMENT

Contour of
pressure
distribution and hub
vortex shape of
tandem propeller at
 $V_{\infty} = 0 \text{ m/s}$

Before modification



After modification

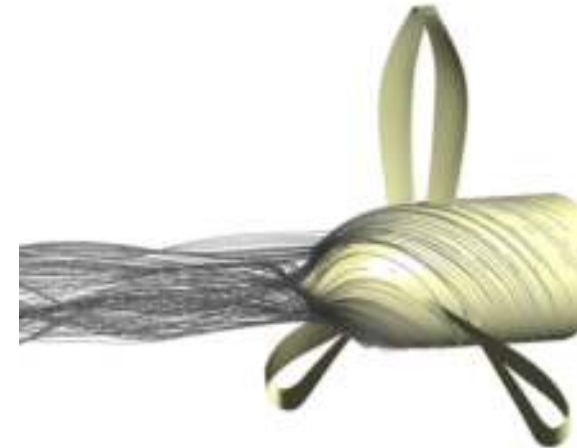
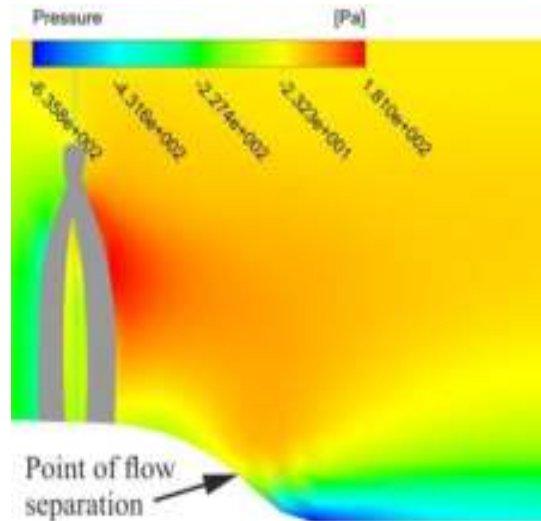




CHARACTERISTICS OF TANDEM PROPELLER AFTER MODIFICATION AND OPTIMIZATION PROFILE ARRANGEMENT

Contour of
pressure
distribution and hub
vortex shape of
tandem propeller at
 $V_{\infty} = 25 \text{ m/s}$

Before modification



After modification

